



PHOTOCATALYTIC CONVERSION OF CO₂ INTO RENEWABLE FUELS: MATERIAL AND REACTOR DESIGN

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Supporting Information*

ABSTRACT. Photocatalytic conversion of CO₂ by using sustainable sunlight energy to convert CO₂ greenhouse gas to renewable fuels has received increasing interest. This idea could simultaneously solve both problems of global warming and sustainable energy shortage. Several types of photocatalyst material and reactor for photocatalytic CO₂ reduction for realizing solar fuels have been developed extensively. Emphasis is given to both TiO₂-based and non-TiO₂-based materials. Among photocatalysts, salt composites and zeolitic imidazolate frameworks, which are economical material, have exhibited outstanding photocatalytic efficiencies. For the reactor, an internally illuminated monolith reactor has performed an excellent photocatalytic activity. The critical challenges, prospects and the need to give more attention to the design of photocatalyst and reactor for solar energy conversion of CO₂ into renewable fuels have been highlighted successfully.

KEYWORDS: reactor, photocatalyst material, renewable fuel, photocatalytic conversion, carbon dioxide (CO₂)

1. INTRODUCTION

Nowadays, warming of climate change and energy shortage are some of the most significant challenges for humanity [1]. On the one hand, carbon dioxide (CO₂) and other key greenhouse gases (methane, nitrous oxide, and fluorinated gases), which are accumulating in Earth's atmosphere, has been linked to climate change. On the other hand, the energy shortage is also a global issue since the capacity of fossil fuels could not cover the ongoing expansion of the world energy demand. Noting that excessive use of fossil fuels is also considered as a critical cause of global climate change. Therefore, there is an urgent need for finding alternative energy sources for sustainable economic growth [2].

There is a growing interest in the use of CO₂ as the most abundant and economic carbon-containing sources for the development of alternative energy [3]. Typically, the CO₂ utilization processes are classified into four groups (as seen in Table 1), including biocatalytic [4-6], catalytic [7-10], photocatalytic [11-14] and electrocatalytic [15, 16] processes. The idea to drive photocatalytic reactions by using renewable solar energy for converting CO₂ waste gas pollution into substitute fuels provides a viable solution. This promising approach not only reduces CO₂ emission but also simultaneously recycles it as renewable fuel by harvesting readily available solar energy. Among many factors, the presence of efficient photocatalysts plays an essential role in determining the photocatalytic efficiency. On the other approach, enhancing of light harvesting, reducing of photon losses and charge carrier recombination have received attention for the design of a more effective reactor [17, 18].

Herein, we review the research advances made in the design and development of photocatalyst material, and reactor for photocatalytic conversion of CO₂. Different types of photocatalyst, reactor configurations affecting the yield and distribution of products are discussed.

2. PHOTOCATALYST MATERIAL

One of the most significant approach to improve efficiency is to develop and design new photocatalyst. Emphasis is given to TiO₂-based materials with many advantages, such as cheap, nontoxic, chemical stability, and resistant to photo-corrosion [19]. However, the TiO₂ properties, such as relatively large band-gap energy and rapid electron-hole

recombination, should be improved. Hence, to utilize solar radiation for photo-conversion of CO₂, two approaches have been employed as follows:

2.1. Modified TiO₂-based materials

Several methods to develop visible light response TiO₂ photocatalysts, including cation doping (Fe, Co, Ni, Mn, V, Cu, and Zn, etc.), anion doping (carbon (C), boron (B), Sulphur (S) and nitrogen (N)), semiconductors coupling (CdS, Cu₂O, FeTiO₃ and CuFe₂O₄, etc.), and surface alkali/base modification, are proposed and summarized in Table 2 [20-29]. As expected, modified TiO₂, compared with pristine TiO₂, shows a better absorb photons ability in the visible region and a lower rate of electron-hole recombination, resulting in achieving better photocatalytic performance. In/TiO₂ performs the best photocatalytic activity (up to 578 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of CH₄) [20]. N₂H₄/TiO₂ could achieve 416 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of CH₃OH [28]. Recent approaches using five surface modification methods for enhancing photocatalytic CO₂ reduction performance of TiO₂, including impurity doping, metal deposition, alkali modification, heterojunction construction, and carbon-based material loading, are also reviewed [30]. Each of these techniques has its advantages and disadvantages; hence, to combine different modification methods might be a good idea to balance the advantages and disadvantages, resulting in developing more efficient TiO₂-based photocatalysts.

2.2. Non-TiO₂ based materials

Non-TiO₂ based photocatalysts are categorized into three groups depending on their structure/chemical nature [31]. The first category includes single-metal oxides, mixed-metal oxides, metal oxide composites, layered double hydroxides (LDHs) and salt composites. The second category (carbon-based semiconductors) consists of graphene-based composites, carbon nanotube (CNT) composites, g-C₃N₄ composites. Lately, a third category that of hybrid organic-inorganic photocatalytic materials - Zeolitic imidazolate frameworks (ZIFs). Among carbonaceous hybrids, hexamolybdate clusters Cs₂Mo₆Bri₈Bra₆/GO) exhibit the

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best photocatalytic activity (up to 69 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of CH₃OH) [32]. Single-metal oxides, mixed-metal oxides, and metal oxide composites could produce up to 170 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of CH₃OH by Ni [33]. LDHs performs a slightly higher photocatalytic activity, up to 210 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of CH₃OH by Cu-Ni-Al LDH [34]. ZIFs could achieve 342 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of CH₃OH by orthorhombic copper (II) imidazolate frameworks [35]. Importantly, salt composites exhibit excellent photocatalytic activity (up to 526 $\mu\text{mol}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ of C₂H₄O₂ (methyl formate)) by cubic CdIn₂S₄ microspheres [36].

Among photocatalysts, salt composites and ZIFs, which are economical materials, have exhibited outstanding photocatalytic efficiencies. However, the derived photo-efficiency is still relatively low and its comparative impracticality for commercial applications. In addition to an efficient semiconductor photocatalyst for increasing the effectiveness of photocatalytic performance, designing and developing a new reactor for the photo-reduction of CO₂ would be beneficial.

3. REACTOR DESIGN

The reactor is integral to the photocatalysis process and constitutes a vital engineering factor. Some key parameters determine the types of reactor, such as the phases involved (single phase (gas, liquid), multiphase (gas-liquid, gas-solid, liquid-solid, gas-liquid-solid)), the mode of hydrodynamic operation (batch, semi-batch, or continuous), the mixing and flow characteristics (completely mixed, some back-mixing, plug flow, non-ideal flow characteristics), the geometric configuration (dimensions and shape), the light source specifications (output power, spectral distribution, shape, dimensions, operating and maintenance requirements), and the radiation source configuration relative to the reaction space [37, 38]. Several reactor types for photocatalytic conversion of CO₂ to produce solar fuels are summarized in Table 3 [39-54].

3.1. Slurry reactor

First, a slurry reactor with a suspended catalyst has been employed extensively for CO₂ photo-reduction [39-42]. These fundamental studies aimed to either derive kinetic data or design a large reactor. This type of reactor offers many advantages such as (1) a simple construction and a lower investment for a large-scale reactor, (2) the possibility for a large-capacity design, and (3) the low amount of photocatalyst used. Very early, Inoue et al. reported the photocatalytic reduction of CO₂ in a glass cell [39]. Fujiwara et al. experimented with a closed pyrex tube (8 mm in diameter) [40]. Similarly, Grodkowski and Neta used a pyrex bulb (43 mL in volume) [41]. Lu et al. experimented with a 358-mL cylindrical glass vessel [42]. Lee et al. used a tubular glass reactor [55]. Yang et al. designed a stirred-batch annular quartz reactor, as shown in Figure 1 [43]. This reactor could be used as an aqueous NaOH solution with continuous CO₂ bubble flow under light irradiation. Wu et al. conducted a photocatalytic reaction in a slurry batch reactor under saturated CO₂ absorption [44]. However, it notes that slurry-type reactor has many disadvantages including the separation of photocatalyst particles from the reaction mixture, low possibility of photocatalyst recycling, inefficient distribution of light throughout the system, and the challenge of product separation.

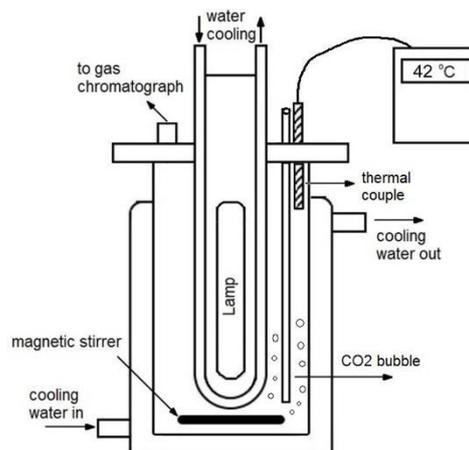


Figure 1. Schematic of a stirred batch annular quartz reactor. (Reprinted from H.-C. Yang et al./ *Catal. Lett.* (2009) 131: 381)

3.2. Fixed-bed reactor

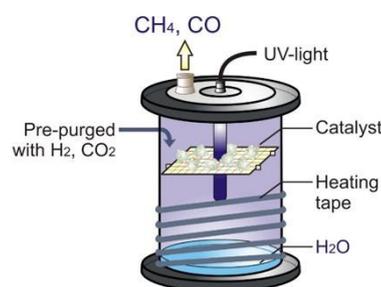


Figure 2. Schematic of a pyrex single reactor system. (Reprinted from B.-R. Chen et al./ *Phys. Chem. Chem. Phys.*, 2016, 18, 4942-4951)

The fixed-bed reactor has various advantages over traditional slurry reactors, such as (1) a higher throughput because of the higher gas velocity and (2) the possibility to immobilize catalysts onto fixed supports, thereby avoiding the drawback of catalyst separation [45-47]. A closed-circulation gas reactor, proposed by Yamagata et al., was also considered for CO₂ photo-reduction [45]. A disc of foam glass, placed inside the reactor, was used to load the photocatalyst. Zhang et al. also designed a fixed-bed reactor for the photo-reduction of CO₂ using a Pt/TiO₂ photocatalyst [46]. A flat quartz glass plate was integrated into the tube to hold the photocatalyst. The reactor (265 mL) measured 400 mm (length) × 35 mm (outside diameter). In another study, Tan et al. developed a new fixed-bed photocatalytic reactor [47]. A cylindrical quartz tube reactor was integrated with a flat glass tray to hold the catalysts. The reactor measured 300 mm (length) × 74 mm (outside diameter) × 3.0 mm (thickness). Moreover, Lo et al. designed a circulated reactor that could provide a fairly high specific surface area and uniform gas concentrations inside the reactor [48]. This reactor was made from a quartz tube with a length of 480 mm and an internal diameter of 22.5 mm. Pyrex glass pellets (3.0 mm in diameter) pre-immobilized with a powder photocatalyst were packed inside the reactor. Recently, a single pyrex reactor (385 mL in volume) was designed for the photocatalytic hydrogenation of CO₂ with H₂O (Figure 2) [49]. A flat teflon surface fixed in the middle of the reactor was used to place the photocatalyst powder evenly.

In another study, the design of a reactor for more efficient photo hydrogenation of CO₂ was addressed by comparing three types of reactors: a gas-phase reactor, a liquid-phase reactor, and a gas-liquid-phase reactor [56]. In the gas-phase

system, a cylindrical tube reactor (pyrex, 260 mL) was used with a quartz plate (92 mm × 40 mm × 2 mm) to pack the photocatalyst. For the liquid-phase system (pyrex, 385 mL), the photocatalyst was suspended in the liquid phase by stirring. The gas-liquid-phase system was very similar to the liquid-phase system and was combined with a teflon plate. The highest quantum efficiency was achieved using the gas-liquid-phase reactor (1.1×10^{-3} %), whereas the efficiency levels of the gas- and liquid-phase systems were only 0.1×10^{-3} % and 0.5×10^{-3} %, respectively. Both H_2 in the gas phase and the proton in the liquid phase could be utilized simultaneously, which contributed to the efficiency enhancement. However, the overall efficiency of the reaction was still very low. A low surface-to-volume ratio and an inefficient light distribution due to the geometry of the light source and the distance between the light source and the photocatalysts resulted in poor interaction between the reactants and the photocatalyst. The above-mentioned is the main issue for this type of reactor [57].

3.2.1. Optical-fiber reactor

In another approach, researchers improved the transmission and distribution of light energy. A first optical-fiber reactor was introduced by Hofstadler and Bauer for photocatalytic wastewater treatment using TiO_2 immobilized on fused-silica glass fibers [58]. The reactor comprised many fibers serving as a medium to effectively and uniformly deliver light to the photocatalyst surface. An optical-fiber reactor has been successfully used for the photocatalytic reduction of CO_2 in a steady-state flow system [13, 50, 51, 59-62]. Figure 3 presents a schematic and a photograph of an optical-fiber reactor (216 mL in volume) with 216 catalyst-coated optical fibers (110 mm in length) [50].

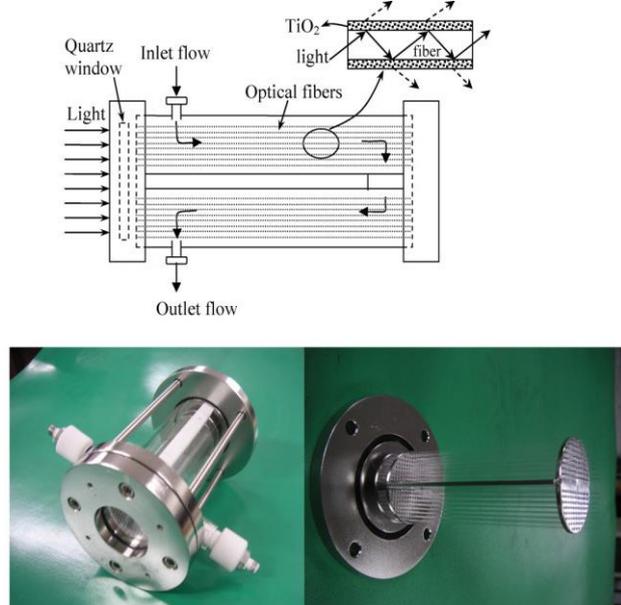


Figure 3. Schematic and a digital photograph of an optical-fiber reactor. (Reprinted from T.-V. Nguyen, J.C.S. Wu/ *Appl. Catal. A* 335 (2008) 112–120)

The photocatalyst-coated optical fibers were assembled in the reactor so that the light source could enter along the fibers

to induce the photocatalytic reaction on its surface. Notably, the transformation of CO_2 to hydrocarbons using sunlight is one of the best routes to producing renewable energy. Nguyen et al. synthesized a metal-doped TiO_2 catalyst sensitized with $Ru(II)(2,2'$ -bipyridyl-4,4'-dicarboxylate) $2-(NCS)_2$ (N3 dye), which was employed to photo-reduce CO_2 with H_2O under concentrated natural sunlight in an optical-fiber reactor [51]. The optical-fiber reactor provides a medium to transmit light uniformly throughout the reactor, compared with a traditional packed-bed reactor and consequently increases the photo-conversion efficiency. However, one of the disadvantages to this type of reactor is that it does not effectively utilize the entire reactor volume. Because a photocatalyst is coated on optical fibers that are usually thin and constitute only 20-30 % of the reactor volume, it provides a relatively low surface area for the coating support.

3.2.2. Monolith reactor

To solve the mentioned concerns, a monolith reactor which provides (1) a large ratio of illuminated surface area to reactor volume and (2) efficient light utilization/ distribution over the photocatalyst surface, could be advantageous. The specific surface area of a monolith (also called honeycomb) is 10-100 times higher than that of other types of catalyst support [63]. Various photocatalysts are prepared to load the monolith channels by using sol-gel dip-coating methods, including N/TiO_2 and Cu/TiO_2 [64], $Cu-In/TiO_2$ [65], In/TiO_2 [52], $NiO/InTaO_4$ [53], Pd/TiO_2 and Rh/TiO_2 [54], Mn/TiO_2 [66], and Ag/TiO_2 [67]. Recently, a monolith reactor comprising a stainless steel cylindrical vessel (5.5 cm in length, 150 mL in volume) was designed, as illustrated in Figure 4 [52]. The quantum efficiency of this monolith reactor was 200 times higher than that of a cell-type reactor. The significant improvement in the monolith reactor was attributed to a higher illuminated surface area, higher photon energy consumption, and better reactor volume utilization, compared with a cell-type reactor.

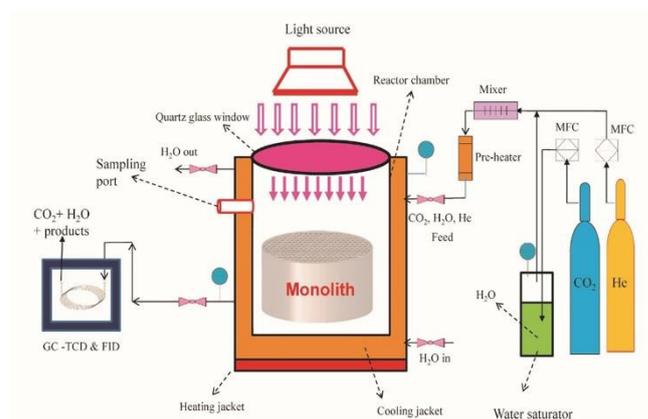


Figure 4. Schematic of an experimental setup using a monolith reactor. (Reprinted from M. Tahir and N.-S. Amin/ *Appl. Catal. A* 467 (2013) 483–496)

3.2.3. Internally illuminated monolith reactor

Furthermore, an internally illuminated monolith reactor is successfully designed and assembled to perform photocatalytic CO_2 reduction (Figure 5) [53].

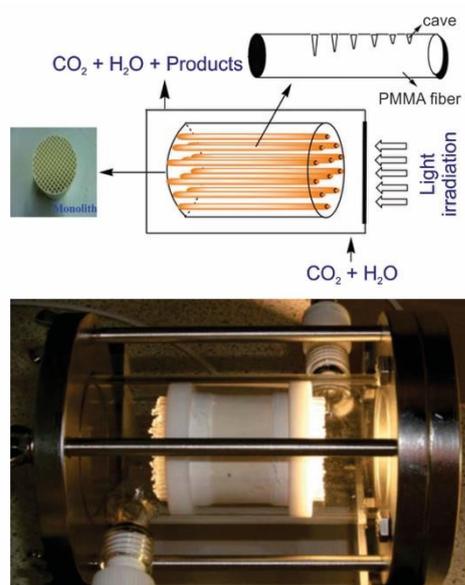


Figure 5. Schematic and digital photograph of an internally illuminated monolith reactor. (Reprinted from P.-Y. Liou et al./ *Energy Environ. Sci.*, 2011, 4, 1487–1494)

A uniform NiO/InTaO₄ layer was obtained from the top of a pre-coated SiO₂ sublayer on the internal channels of the monolith. The monolith structure could significantly increase the number of catalysts loaded due to the multiple channels. The carved optical fibers were inserted to transmit and scatter light to illuminate the catalyst inside the monolith channels. Recently, Ola et al. conducted and compared the performance of CO₂ photocatalytic reduction in a slurry batch annular reactor and an internally illuminated monolith reactor [54]. Due to the combined advantages of both the monolith (high surface area) and the optical fibers (uniform light distribution), the quantum efficiency of the internally illuminated monolith reactor was 23.5 times higher than that of the traditional slurry batch annular reactor. A reactor with high quantum efficiency will play an essential role in a commercial scale-up application for producing solar fuels in the future.

3.3. Membrane reactor

Membrane reactor type (twin-reactor) is promoted to combine photocatalytic water-splitting and CO₂ hydrogenation. This design is combined between slurry and fixed-bed reactors (as seen in Fig. 6). There are two major advantages in the membrane reactor. Firstly, CO₂ could be directly hydrogenated to hydrocarbons by the produced H₂. Secondly, the separation of H₂ and O₂ prevents the backward reaction of water splitting and the oxidation of the produced hydrocarbons by O₂ back into CO₂. Applying the membrane reactor could improve both photo-reduction quantum efficiency (PQE) and the selectivity for CO₂ reduction (SCR) [68]. Membrane reactor performs PQE more than four folds from 0.015 % to 0.070 %, compared with the slurry reactor. The SCR in the membrane reactor reaches to 99.1 % which is higher than that in the slurry reactor (73.6 %). Despite the noticeable results achieved, there is a need for further improving the efficiency of photocatalytic CO₂ hydrogenation. The bottleneck is the limited efficiency of the H₂-generating.

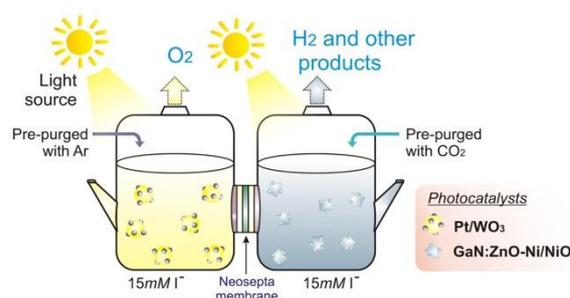


Figure 6. Schematic of the membrane reactor. (Reprinted from Yu et al./ *Appl. Catal. A* 518 (2016) 158–166)

4. SUMMARY AND FUTURE PERSPECTIVES

In summary, the approach of converting the CO₂ greenhouse gas into renewable fuels using sunlight is considered a viable solution to simultaneously solve global warming and sustainable energy shortage problems. Several photocatalyst materials, reactor types have been designed for photocatalytic conversion of CO₂ to produce solar fuels. Among photocatalysts, salt composites and ZIFs, which are economical materials, have exhibited outstanding photocatalytic efficiencies. It is noted that the optimization of the operating conditions, such as temperature, pressure, and light, plays a vital role in achieving a good yield and product selectivity. Among reactor types, an internally illuminated monolith reactor performs an excellent photocatalytic activity. It showed a 23.5-fold increase in quantum efficiency compared to the traditional slurry reactor. Because low surface-to-volume ratios and inefficient light distribution are the primary concerns during the design of the reactor, additional studies must focus more on (1) improving the geometrical arrangement of the radiation source relative to the reaction space and (2) increasing the illuminated surface area to reactor volume.

From our point of view, photocatalytic conversion of CO₂ is promising and potentially feasible technology that not only convert sunlight energy into solar fuels but also reduce atmospheric CO₂; however, their efficiency is still relatively low and far away from the benchmark photo-conversion efficiency for commercialization. The reason is that photocatalysts and their experimental conditions, such as the nature of the reactors, reaction temperature, pressure, and light source specifications, have not been well optimized. To further enhance the photocatalytic performance, emphases are given to:

- (1) Continually develop more efficient photocatalysts with higher mechanical and chemical stabilities and a broader optical absorption band while slowing down the undesirable recombination of e⁻/h⁺ pairs;
- (2) Focus on elucidating mechanisms, surface reaction pathways, electron transfer dynamics, and reaction intermediates through in-situ spectroscopic techniques (XANES, FT-IR, Raman), carbon isotopes (¹³C-labeled CO₂) supported by theoretical studies to explain the formation of various products;
- (3) Systematically develop and explore models simulating the performance of the reactor;
- (4) Understand the optical properties and geometrical arrangement of the radiation source relative to the reaction space in different reactor systems.

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Table 1. Summary of advantages and disadvantages for catalytic CO₂ reduction processes

No.	Catalytic process	Advantages	Disadvantages
1	Biocatalytic	+ High efficiency; + None toxicity; + Excellent biodegradability; + Possibility to synthesize liquid fuels	+ Cumbersome process
2	Catalytic (Heterogeneous catalysis)	+ Excellent performance, efficiency; + Easy recyclability	+ High temperature requirement; + Low selectivity
	Catalytic (Homogeneous catalysis)	+ Excellent performance, efficiency; + High selectivity.	+ Separation concern for reaction product; + Not stable toward heat and pressure; + Difficult recyclability.
3	Photocatalytic (Heterogeneous photocatalysis)	+ Artificial photosynthesis for storage of solar energy; + A cost-competitive, safety and eco-friendly alternative toward solar fuels; + Easy recyclability	+ Low efficiency
	Photocatalytic (Homogeneous photocatalysis)	+ Artificial photosynthesis for storage of solar energy; + A cost-competitive, safety and eco-friendly alternative toward solar fuels	+ Separation concern for reaction product; + Difficult recyclability.
4	Electrocatalytic	+ Possibility to directly synthesize liquid fuels (long-chain molecule)	+ High energy barrier

Table 2. Summary of performance under different modification techniques for TiO₂.

No.	Modification techniques	Photocatalysts	Reaction Conditions	Products	Yield	Ref.
1	cation doping	TiO ₂	Halogen lamp (500W; 380-1100 nm; 68.35 mW·cm ⁻²);	CH ₃ OH	No product formation;	[21]
		V/TiO ₂			1.2 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
		Cr/TiO ₂			0.7 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
		Co/TiO ₂			1.6 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
2		TiO ₂	Mercury flash lamp (500W; 365 nm; 40 mW·cm ⁻²);	CH ₄	36.5 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[20]
		In/TiO ₂			578 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
3		TiO ₂	Four UV bulbs (8W; 365 nm; 3.25 mW·cm ⁻²);	CH ₄	0.5 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[22]
		Ag/TiO ₂			2.6 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
4		TiO ₂	White light LED (30W; 400–455 nm);	CH ₄	0.4 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[23]
		Au/TiO ₂			4.9 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
5	anion doping	TiO ₂	The compact fluorescent integrated bulbs (Philips Tornado: 6 bulbs; 13W; 400-800 nm; 0.37 mW·cm ⁻²);	CH ₄	0.05 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[24]
		N/TiO ₂			0.15 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
6	semiconductors coupling	TiO ₂	Mercury lamp (125W; 350-400 nm);	CH ₄	No product formation;	[25]
		CdS/TiO ₂			0.19 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
7		TiO ₂	High-pressure Xe lamp (500W; < 300 nm);	CH ₃ OH	0.17 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[26]
		FeTiO ₃ /TiO ₂			0.47 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
8	surface alkali/base modification	MgO/TiO ₂	Oriel Xe lamp (400W; 200-1000 nm; 420 mW·cm ⁻²);	CO	4.0 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[27]
		MgO/TiO ₂			37.5 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
9		TiO ₂	Visible light sources (300W; UV < 5%; 420 mW·cm ⁻²);	CH ₄	6.9 ppm·g _{cat} ⁻¹ ·h ⁻¹ ;	[28]
		N ₂ H ₄ /TiO ₂			416 ppm·g _{cat} ⁻¹ ·h ⁻¹ ;	
		NH ₃ /TiO ₂			338 ppm·g _{cat} ⁻¹ ·h ⁻¹ ;	

Table 3. Summary of photocatalytic reduction and hydrogenation of CO₂ for producing solar fuels

No.	Reactor	Photocatalyst	Experiment setup	Light source	Main Products	Ref.	
1	A glass cell	TiO ₂	Purified water (100 ml) contained 1 g photocatalyst was bubbled by CO ₂ gas (3 l·ml ⁻¹).	High-pressure Hg arc lamp (500 W)	HCHO: 1.6×10 ⁻⁴ M·h ⁻¹ ; CH ₃ OH: 3.3×10 ⁻⁵ M·h ⁻¹ ;	[39]	
2		ZnO					HCHO: 1.7×10 ⁻⁴ M·h ⁻¹ ; CH ₃ OH: 0.5×10 ⁻⁴ M·h ⁻¹ ;
3		CdS					HCHO: 2.9×10 ⁻⁴ M·h ⁻¹ ; CH ₃ OH: 1.7×10 ⁻⁴ M·h ⁻¹ ;
4		GaP					HCHO: 1.4×10 ⁻⁴ M·h ⁻¹ ; CH ₃ OH: 1.6×10 ⁻⁴ M·h ⁻¹ ;
5		SiC					HCHO: 1.4×10 ⁻⁴ M·h ⁻¹ ; CH ₃ OH: 7.6×10 ⁻⁴ M·h ⁻¹ ;
6	A closed pyrex tube	ZnS	A DMF solution (2 mL) containing 10mM (diatomic) of ZnS nanocrystallites and 1 M of distilled triethylamine (TEA) was saturated with CO ₂ for photo-redox reactions.	A high-pressure Hg lamp (500 W; λ > 290 nm)	CO: 12.4 μmol·h ⁻¹ ; HCOO ⁻ : 9.4 μmol·h ⁻¹ ; H ₂ : 7.4 μmol·h ⁻¹ ;	[40]	
7	A pyrex bulb	CoTTP	An acetonitrile/methanol (9/1 v/v) solutions containing p-terphenyl (TP, 3 mmol·l ⁻¹) as a photosensitizer, trimethylamine (TEA, 5 %) as a reductive quencher, and 0.05 mmol·l ⁻¹ Co complex.	Xe lamp	CO: 0.41 mmol·l ⁻¹ ; H ₂ : 0.92 mmol·l ⁻¹ ; CO: 2.25 mmol·l ⁻¹ ; H ₂ : 3.44 mmol·l ⁻¹ ;	[41]	
8		hydroxocobalamin					
9	A cylindrical glass vessel	V, N co-doped TiO ₂ nanotube arrays (TNAs)	TNAs films were placed in the center before sealing the reactor contained 20 ml 0.1 mol·l ⁻¹ KHCO ₃ solution.	Hg lamp (300 W)	CH ₄ : 64.5 ppm·cm ⁻² ·h ⁻¹ ;	[42]	
10	A stirred batch annular quartz reactor	TiO ₂ /SBA-15	550 ml aqueous 0.1 N NaOH solution containing about 0.05 g catalyst at 315 K. CO ₂ gas was bubbled into the reactor continuously, and the pH value was kept near pH 7 during the reaction.	Medium-pressure metal halide lamp (400 W, Philips HPA400, 365 nm)	CH ₃ OH: 627 μmol·g ⁻¹ ·h ⁻¹ ; CH ₃ OH: 690 μmol·g ⁻¹ ·h ⁻¹ ;	[43]	
11		Cu/TiO ₂ /SBA-15					
12	A slurry batch reactor	Mo-doped TNTs (Mo-T-500)	Photocatalyst (0.1 g) was loaded in 300 ml of 0.2 M MEA solution contained 0.1 g at the saturated absorption of CO ₂ . The reaction temperature was controlled at 298±2 K.	UVC lamp (8 W; 365 nm; 63 W·cm ⁻²)	CH ₄ : 0.52 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CO: 10.41 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; PQE: 0.22 %.	[44]	
13	A closed circulation gas reactor	TS-1	The prior reaction, photocatalyst (20 mg) was activated by UV irradiation under an H ₂ atmosphere (1.0×10 ⁵ Pa). After H ₂ was evacuated, reactant gas was introduced (1.0×10 ⁵ Pa).	Hg lamp (Ushio ML-251 A/A)	CH ₄ : 7.8×10 ⁻⁸ mol·h ⁻¹ ;	[45]	
14	A fixed-bed reactor	Pt/ TiO ₂ nanotube	The reaction was carried out with catalysts (50 mg), CO ₂ (99.5% purity) and H ₂ O vapor. The amount of H ₂ O vapor depended on the H ₂ O/CO ₂ molar ratio, which was regulated by the temperature in the conical flask.	High-pressure Hg lamp (300 W, 365 nm)	CH ₄ : 4.8 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 3.9 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[46]	
15		Pt/ TiO ₂ (P25)					
16	A fixed-bed reactor	TiO ₂ pellets: JRC-TiO-4	TiO ₂ pellets (100 g) was spread out on the flat tray in the reactor.	NEC Germicidal	CH ₄ : 1.4×10 ⁻² μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[47]	

17		TiO ₂ pellets: porous Vycor glass (PVG)	The reactants included water (vapor) and highly purified (99.999%) CO ₂ gas.	lamps (1.6 W; GL8; 253.7 nm)	CH ₄ : 2.5×10 ⁻³ μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
18		TiO ₂ pellets: Aerolyst 7708			CH ₄ : 2.1×10 ⁻³ μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
19	A circulated reactor	TiO ₂ immobilized Pyrex glass pellets	+ CO ₂ (99.8 %, SUPELCO Scott Specialty Gases, Cat. No. 501298): 5 %; + H ₂ (99.995 %): 90 %; + H ₂ O (D.I. water): 5 %;	A near-UV fluorescent black lamp (4×15 W; Sankyo Denki Co. Ltd., Japan; F10TBLB; 365 nm)	CH ₄ : 4.11 mmol·g _{cat} ⁻¹ ·h ⁻¹ ; CO: 0.14 mmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₆ : 0.10 mmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[48]
20	A single pyrex reactor	Cu/TiO ₂	H ₂ O (5 mL), H ₂ (0.01 atm), saturated CO ₂ (1 atm); 363 K	11SC-1 pen-ray lamp (12 mW cm ⁻² ; 254 nm)	CO: 0.54 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 3.59 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; PQE: 0.13 %;	[49]
21			H ₂ O (5 mL), saturated CO ₂ (1 atm)		CO: 0.03 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 0.67 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; PQE: 0.03 %;	
22	An optical-fiber reactor	Cu(0.5 wt%)-Fe(0.5 wt%)/TiO ₂ / glass plate	The reactor was purged by CO ₂ gas bubbling through D.I. water for 1 h at 348 K. The space velocity of the CO ₂ gas and H ₂ O vapor was maintained at 0.72 h ⁻¹ .	High pressure Hg lamp (150 W; 225 mW·cm ⁻² ; 320–500 nm)	C ₂ H ₄ : 0.05 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 0.06 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[50]
23		Cu(0.5 wt%)-Fe(0.5 wt%)/TiO ₂ / optical fiber			C ₂ H ₄ : 0.05 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 0.06 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
24	An optical-fiber reactor	N3-dye-Cu(0.5 wt%)-Fe(0.5 wt%)/TiO ₂	The reactor was purged by CO ₂ gas bubbling through D.I. water for 1 h at 348 K. The space velocity of the CO ₂ gas and H ₂ O vapour was maintained at 0.72 h ⁻¹ .	Concentrated natural sunlight (20 mW·cm ⁻²)	CH ₄ : 0.62 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[51]
25	A monolith reactor	TiO ₂ -cell	P _{CO2} = 0.040 bar, P _{H2O} = 0.074 bar, T = 373 K.	Hg lamp (200W; 150 mW·cm ⁻² ; 252 nm)	CO: 5.20 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 7.70 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₄ : 0.79 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	[52]
26		TiO ₂ -monolith			CO: 43.00 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 78.00 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₄ : 1.50 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₆ : 0.79 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
27		In/TiO ₂ -monolith			CO: 962.00 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; CH ₄ : 55.40 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₄ : 0.34 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₆ : 1.50 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₃ H ₆ : 0.07 μmol·g _{cat} ⁻¹ ·h ⁻¹ ;	
28	An internally illuminated monolith reactor	1%NiO/InTaO ₄ (sg)	Vapor-phase CO ₂ with saturated H ₂ O was photo-reduced to hydrocarbons by UV or visible-light in a steady-state flow.	Xenon lamp, visible light 42.46 mW·cm ⁻²	CH ₃ OH: 0.16 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; QE: 0.012 %;	[53]
29		1%NiO/InTaO ₄ (sg)		Mercury lamp, UVA light 42.46 mW·cm ⁻²	C ₂ H ₄ O: 0.3 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; QE: 0.057 %;	
30		2.6%NiO/InTaO ₄ (imp)		Xenon lamp, AM1.5G 100 mW·cm ⁻²	C ₂ H ₄ O: 0.3 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; QE: 0.058 %;	
31	A slurry batch	1 wt% Pd/0.01 wt% Rh-TiO ₂	200 ml of D.I. water contained 1 g photocatalyst was magnetically stirred at 240 rpm. Ultra-pure	UVA lamp (2×8 W; Sylvania; 3.22	CH ₄ : 0.03 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; QE: 0.002 %;	[54]

	annular reactor		CO ₂ (Air Products, 99.999%) gas was bubbled at 1 bar for 35 min then the CO ₂ supply was cut off.	mW·cm ⁻² ; 365 nm)		
32	An internally illuminated monolith reactor		The reactor was then purged with He for 1 h, then switched to CO ₂ gas saturated with H ₂ O vapor for 1 h at a flow rate of 4 ml/min. The retention time (volume/flow rate) of the monolith was 54 min. The flow of CO ₂ saturated with water vapor was continuous throughout the reaction.	High pressure Hg lamp (Exfo Omnicure S1500; 41.62 mW·cm ⁻² ; 320–500 nm;	CH ₃ OH: 0.10 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; C ₂ H ₄ O: 0.21 μmol·g _{cat} ⁻¹ ·h ⁻¹ ; QE: 0.062 %;	